

# X-HVB Nailed Shear Connector

# Design according to AS/NZS 2327:2017

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- 1. Hilti X-HVB Nailed Shear Connector Design according to AS/NZS 2327:2017
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3. European Technical Assessment ETA-15/0876 of 3 June 2016: Nailed shear connector X-HVB



September 12, 2019



# Hilti X-HVB Nailed Shear Connector Design according to AS/NZS 2327:2017

# SUMMARY

The purpose of this document is to summarize technical information on the use of Hilti X-HVB nailed shear connector in accordance with the new Australian/New Zealand composite construction standard AS/NZS 2327:2017 [1].

The design capacities of the X-HVB as provided in the European Technical Assessment ETA-15/0876 [2] can be also used in the Australian and New Zealand market. The corresponding assessment was made by HERA – Heavy Engineering Research Association (HERA Report SSTR-066 [3]).

The Hilti X-HVB shear connectors (X-HVB 80, X-HVB 95, X-HVB 110, X-HVB 125 and X-HVB 140) are also included within the "HERA Composite Beam and Slab Software". This document further summarizes the design capacities of the X-HVB used in that software, which are dependent on the different composite deck geometries. Furthermore, X-HVB positioning schemes for these composite decks are specified. Specifically, positioning drawings are provided in Appendix 2 for the ComFlor composite decking types (ComFlor 60, ComFlor 80 and ComFlor SR).

<u>Important note</u>: The user of the "HERA Composite Beam and Slab Software" needs to check separately if the placement of the required number of X-HVB's is possible in the available ribs considering the positioning provisions within the rib.

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# 1 GENERAL DESIGN PROVISIONS

The design resistance P<sub>Rd</sub> of the Hilti nailed shear connector X-HVB is given in the European Technical Assessment ETA-15/0876 [2]. The data within ETA-15/0876 [2] allows design of composite beams in strict compliance with Eurocode 4, EN 1994-1-1 [4].

HERA – Heavy Engineering Research Association – assessed the suitability of using the X-HVB design data of ETA-15/0876 [2] in accordance with the new Australian/New Zealand Standard AS/NZS 2327:2017 [1]. The performance of the X-HVB in the context of AS/NZS 2327:2017 [1] is described in detail in the HERA Report SSTR-066 [3].

The key conclusions for the design of Hilti X-HVB nailed shear connectors related with AS/NZ 2327:2017 [1] are:

- The design resistance P<sub>Rd</sub> as given in Annex C1 and Annex C2 of ETA-15/0876 [2] can be equivalently applied as design shear capacity P<sub>Rd</sub> per AS/NZS 2327:2017 [1].
- The same level of safety on the resistance is applied. ETA-15/0876 [2] uses the partial factor  $\gamma_V = 1.25$  from EN 1994-1-1 [4], whereas AS/NZS 2327 [1] applies a capacity factor  $\phi = 0.8$ . Therefore, the characteristic resistance P<sub>Rk</sub> as given in Annex C1 of ETA-15/0876 [2] for solid concrete slab can be equivalently applied as nominal shear capacity P<sub>Rk</sub> per AS/NZS 2327:2017 [1].
- The design data of ETA-15/0876 [2] can be equivalently applied for steel base materials with nominal yield strength f<sub>y</sub> of 235 to 355 N/mm<sup>2</sup>.
- The design data of ETA-15/0876 [2] can be equivalently applied for characteristic concrete strength fc' = 20 to 50 N/mm<sup>2</sup>.

Table 1-1 summarizes the calculation of the design shear capacity of the X-HVB nailed shear connector per AS/NZS 2327:2017 [1] and compares it with the nomenclature of EN 1994-1-1 [4].

Parameter	AS/NZS 2327:2017 [1]	EN 1994-1-1 [4]				
	$P_{Rd} = \phi P_{Rk}$	$P_{Rd} = \frac{P_{Rk}}{\gamma_V}$				
Design data	$P_{Rd}$ Design shear capacity $P_{Rk}$ Nominal shear capacity $\phi$ capacity factor ( $\phi$ = 0.8)	$P_{Rd}$ Design resistance $P_{Rk}$ Characteristic resistance $\gamma_V$ Partial factor ( $\gamma_V$ = 1.25)				
	The X-HVB is considered as ductile shear connector.	The X-HVB is considered as ductile shear connector.				
	The values $P_{Rk}$ and $P_{Rd}$ apply per ETA-15/0876 [2].					
	The presence of composite decking is considered by application of the reduction factors $k_{t,l}$ , $k_{t,t}$ or $k_{l}$ .					
Steel grades <sup>1</sup>	Construction steel with nominal yield strength f <sub>y</sub> = 235 to 355 N/mm²	Steel grades S235, S275 and S355 in qualities JR, J0, J2 and K2 (EN 10025-2)				
Concrete strength	f <sub>c</sub> <sup>-</sup> = 20 to 50 N/mm <sup>2</sup>	C20/25 to C50/60				
Conditions per ETA- 15/0876 [1]	<ul> <li>Observation of tool energy setting recommendation per Annex B3<sup>2</sup></li> <li>Observation of application limit<sup>3</sup> and fastener stand-off provisions per Annex B3</li> <li>Observation of geometric parameters per Annex B4</li> <li>Observation of X-HVB positioning rules per Annex B5, B6, B7 and B8</li> </ul>					

#### Table 1-1 Design capacity of X-HVB per AS/NZS 2327:2017 [1]

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<sup>&</sup>lt;sup>1</sup> Thermomechanically rolled steel beams are not covered by the application limit given in Annex B3 of ETA-15/0876 [1], inquire at Hilti.

For base material thickness ≥ 10 mm: Black cartridge 6.8/18M For base material thickness 8 to 10 mm: Black or Red cartridge 6.8/18M For base material thickness 6 to 8 mm: Red cartridge 6.8/18M

<sup>&</sup>lt;sup>3</sup> Note: Thermomechanilly rolled fine grained steel not covered, inquire at Hilti.



# 2 DESIGN SHEAR CAPACITIES USED IN HERA SOFTWARE

# 2.1 STEEL DECKING AND SELECTION PARAMETERS

The Hilti X-HVB shear connectors (X-HVB 80, X-HVB 95, X-HVB 110, X-HVB 125 and X-HVB 140) are also included within the "HERA Composite Beam and Slab Software". This software uses the design method provided in the new Australian/NZ composite construction standard AS/NZS 2327:2017 [1].

The "HERA Composite Beam and Slab Software" includes a set of composite decking used in the Australian and New Zealand market as summarized in Table 2-1.

	Steel decking covered by the Software						
Designation	Shape	Height h <sub>p</sub> [mm]	Overall depth t <sub>p</sub> [mm]	Rib width b₀ [mm]	(b <sub>0</sub> /h <sub>p</sub> ) or (b <sub>0</sub> /t <sub>p</sub> ) [-] (1)	Bottom rib (centre) stiffener	
Formsteel Unifloor, Flatdeck, Tray-deck 300	Rectangular	54, 57, 58	54, 57, 58	na.	na.	No	
Formsteel, Svelte 60	Trapezoidal	60	63	147,5	2,46	Yes	
Formsteel, Svelte 80	Trapezoidal	80	83	147,5	1,84	Yes	
Hibond 80	Trapezoidal	80	95	179,0	1,88	No	
Hibond 55	Trapezoidal	55	55	154,5	2,81	Yes	
Tray-dec 60	Trapezoidal	60	60.75	136,7	2,28	Yes	
Tray-dec 80	Trapezoidal	80	81	149,1	1,86	Yes	
ComFlor 60	Trapezoidal	60	75	144,6	1,93	No	
ComFlor 80	Trapezoidal	80	95	135,0	1,42	No	
ComFlor SR	Re-entrant	55	55	161,0	2,93	No	

#### Table 2-1 Steel decking covered by the "HERA Composite Beam and Slab Software"

(1) for decking with top crest stiffener of 15 mm height (Hibond 80, ComFlor 60 and ComFlor 80), the ratio  $(b_0/t_p)$  is calculated.

Sketches of the geometry of all decking are provided Appendix 1.

#### Important note:

The user of the "HERA Composite Beam and Slab Software" needs to check separately if the placement of the required number of X-HVB's is possible in the available ribs considering the positioning provisions within the rib.



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The "HERA Composite Beam and Slab Software" does not check the geometric requirements related with the positioning of the X-HVBs in the decking rib.

Therefore, a pre-selection of the X-HVB's was prepared by Hilti per decking type.

This pre-selection includes:

- Minimum X-HVB height
- Orientation of the X-HVB in the rib in case of decking transverse to be beam:
  - Parallel to the beam
  - Transverse to the beam
  - Minimum number of X-HVB per rib
- Design capacity in composite beams with solid concrete slab (default X-HVB orientation: longitudinal to the beam)
- Design capacity in composite beams with composite slabs (with decking transverse or parallel with the beam)
  - For 1, 2 and 3 X-HVB's per rib (general case)
  - For 1, 2, 3 and 4 X-HVB's per rib (in the specific case of the use of X-HVB 140 in combination with ComFlor 80 composite decking)

The following sections summarize the X-HVB design capacities and provide information on their calculation. They correspond with the values used by the software. They already consider a potential reduction with the respective reduction factor k:

- kt,I .... decking transverse to the beam and X-HVB longitudinal to the beam
- k<sub>t,t</sub> .... decking transverse to the beam and X-HVB transverse to the beam
- k<sub>1</sub> ..... decking parallel with beam (default X-HVB orientation: longitudinal to the beam)

# 2.2 SOLID CONCRETE SLAB

The same values as given in the ETA-15/0876 [2] apply, those are also summarized in Table 2-2 and in Table 2-3 for reference. The X-HVBs are to be positioning longitudinal with the beam and the geometric provisions as given in ETA-15/0876, Annex B5 [2] are to be observed.



# 2.3 DECKING TRANSVERSE WITH BEAM

Table 2-2 summarizes the conditions and design capacities  $P_{Rd}$  for composite decking transverse with the beam. With the exception of the test based data for the ComFlor 80 decking, all design capacities are calculated per ETA-15/0876 [2] applying the reduction formula from Table 4 in Annex C1 of the ETA-15/0876 [2]. For specific calculation notes see the end of this section.

Table 2-2	Design Data f	or HERA Softw	are. Solid conc	rete slah and c	decking transvers	e with heam
	Design Data n		are. Sonu conc	iele siab anu c	ueching inansvers	e with beam

Composite beam with solid slab or composite decking transverse to beam							[	Design re	esistance	e P <sub>Rd</sub> [kN	]			
Designation	Shape	Height h <sub>p</sub> [mm]	Overall depth t <sub>p</sub> [mm]	Positioning X-HVB vs. Beam	Minimum height	Positiong scheme	Minimum number of X-HVB per rib	Number of X-HVB per rib	X-HVB 80	X-HVB 95	X-HVB 110	X-HVB 125	X-HVB 140	
Solid Slab	*	*	*	Longitudinal	X-HVB 80	А	n.a.	n.a.	26,00	28,00	28,00	30,00	30,00	
Formsteel Unifloor, Flatdeck, Tray-deck 300	Rectangular	54, 57, 58	54, 57, 58	Longitudinal	X-HVB 80	A	1	1 2 3	26,00	28,00	28,00	30,00	30,00	
Formsteel				-		_		2	*	24,73	24,92	26,70	26,70	
Svelte 60	i rapezoidai	60	63	Transverse	X-HVB 95	в	2	3	*	20,19	24,92	26,70	26,70	
Formsteel	Tuonomoidal	00	0.2	Тирина		P	2	2	*	*	*	*	26,70	
Svelte 80	Trapezoidai	80	63	Transverse	X-HVB 140	В	2	3	*	*	*	*	22,20	
								1	*	*	×	*	26,70	
Hibond 80	Trapezoidal	80	95	Transverse	X-HVB 140	С	1	2	*	*	*	*	19,88	
								3	*	*	×	*	16,23	
Hibond 55	Trapezoidal	55	55	Transverse	X_H\/B 05	в	2	2	*	24,92	24,92	26,70	26,70	
Thibolid 35	Паредока	55	55	Transverse	X-110D 33	D	2	3	*	24,92	24,92	26,70	26,70	
Trav-dec 60	Trapezoidal	60	60	Transverse	X-HVB 95	в	2	2	*	24,92	24,92	26,70	26,70	
	Trapozoldal	00	00	Transverse	X1111B 00	5 2	3	*	21,54	24,92	26,70	26,70		
Trav-dec 80	Trapezoidal	80	80	Transverse	X-HVB 125	в	2	2	*	*	*	22,28	26,70	
	Trapozoldal	00	00	Transverse	X1110 120	, D	2	3	*	*	*	18,19	24,39	
								1	*	*	24,92	26,70	26,70	
ComFlor 60	Trapezoidal	60	75	Transverse	X-HVB 110	С	1	2	*	*	18.71	26,70	26,70	
								3	*	*	15,28	23,39	26,70	
								1	*	*	*	*	21,22	
ComFlor 80	Tranezoidal	80	95	Transverse	X-HVB 140		N/D 140	1	2	*	*	*	*	21,22
	Trapozoldal	00	00	Transverse	хнив 140	D		3	*	*	*	*	19,20	
								4	*	*	*	*	17,60	
								1	*	28,00				
ComFlor SR	Re-entrant	55	55	Longitudinal	X-HVB 95	А	1	2	*	27,80	28,00	30,00	30,00	
								3	*	22,70				

#### Positioning scheme (A)

The scheme corresponds with the positioning in solid concrete slabs per Annex B5 of ETA-15/0876 [2].

With regards to the design capacity, flat decks are considered as solid concrete slabs according to AS/NZS 2327: 2017, Clause 3.6.2.4.2. [1]. However, due to the presence of bottom rib stiffeners, the minimum longitudinal spacing – given as 100 mm for solid slabs – might be slightly adjusted, as well as the way of alternating the X-HVB connectors in case of one row of X-HVB connectors.



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#### Positioning scheme (B)

This scheme is recommended for decks with a center bottom rib stiffener as shown in Annex B7 of ETA-15/0876 [2] for 2 or 3 X-HVBs per rib. Sub-scheme b) is recommended:



Scheme b) with X-HVB in the center of half of the rib

#### Positioning scheme (C)

The scheme covers deck without a central rib stiffener as the ComFlor 60 or the HiBond 80. Therefore, the X-HVBs can be placed in transverse orientation in the center of the rib, see Annex B7 of ETA-15/0876 [2] and the relevant extract below. Also, the use of just one X-HVB per rib is possible as the deck mid-height to X-HVB distance exceeds 40 mm.



X-HVB positioning drawings in all 3 ComFlor decking (ComFlor 60, ComFlor 80 und ComFlor SR) are provided in Appendix 2.



### Spacing

Except for ComFlor 80 decking, all decking has a compact geometry as the ratio  $(b_0/h_p)$  or  $(b_0/t_p)$  exceeds the value of 1.8 (see Table 2-1). Therefore, the spacing provisions for compact decking geometries as given in Annex B6 and B7 of ETA-15/0876 [2] apply.

Based on the tests with ComFlor 80 [3], the specific spacing provision for X-HVB 140 and ComFlor 80 are as follows:



#### **Calculation notes**

Decking with small top rib stiffeners (Svelte 60 and Svelte 80) or slight deviation from nominal height (Tray-dec 60 and 80)

- Svelte 60 and Svelte 80:
  - For Svelte 60 the very small stiffeners are considered negligible (see also section 3.6.2.4.2 (c) of [1]) related with the selection of the smallest X-HVB (→ X-HVB 95 for Svelte 60).
  - The stiffeners are conservatively considered in the calculation of the reduction factor  $k_{t,t}$  and the calculation is done with the overall depth  $t_p$ .
- Tray-dec 60 and Tray-dec 80:
  - The very small height deviation (60.75 mm vs. nominal 60 mm / 81 mm vs. 80 mm) is considered negligible related with the selection of the smallest X-HVB (→ X-HVB 95 and → X-HVB 125, respectively).
  - The actual height of 60,75 mm or 81 mm is considered in the calculation of the reduction factor k<sub>t,t</sub>.

Decking with top crest stiffener of 15 mm height

- Hi-Bond 80:
  - The minimum X-HVB height was selected with 140.
  - The stiffeners are conservatively considered in the calculation of the reduction factor  $k_{t,t}$  and the calculation is done with the overall depth  $t_p$  of 95 mm.
- ComFlor 60:
  - The minimum X-HVB height was selected with 110.
  - The stiffeners are conservatively considered in the calculation of the reduction factor k<sub>t,t</sub> and the calculation is done with the overall depth t<sub>p</sub> of 75 mm.
- ComFlor 80: New testing is available per HERA SST-066 [3]. Therefore, the test-based design resistances are directly used for n = 1, 2, 3 and 4.

Decking with rectangular shape (Formsteel Unifloor, Flatdeck, Tray-dec 300)

• The reduction factor  $k_{t,i}$  = 1.0 is applied as given in section 3.6.2.4.2 of [1] for clipped pan profiles.



# 2.4 DECKING PARALLEL WITH BEAM

Table 2-3 summarizes the conditions and design capacities  $P_{Rd}$  for composite decking parallel with the beam. All design capacities are calculated per ETA-15/0876 [2] applying the reduction formula from Table 5 in Annex C2 of the ETA-15/0876 [2].

Table 2-3	Design	Data for H	IERA Sof	ftware: Soli	d concrete	slab and	l deckin	ng paralle	l with b	beam

Composite beam with solid slab or composite decking parallel with beam							Design re	esistance	e P <sub>Rd</sub> [kN	]
Designation	Shape	Height h <sub>p</sub> [mm]	Overall depth t <sub>p</sub> [mm]	Positioning X-HVB vs. Beam	Minimum height	X-HVB 80	X-HVB 95	X-HVB 110	X-HVB 125	X-HVB 140
Solid Slab	*	*	*	Longitudinal	X-HVB 80	26,00	28,00	28,00	30,00	30,00
Formsteel Unifloor, Flatdeck, Tray-deck 300	Rectangular	54, 57, 58	54, 57, 58	Longitudinal	X-HVB 80	26,00	28,00	28,00	30,00	30,00
Formsteel, Svelte 60	Trapezoidal	60	63	Longitudinal	X-HVB 95	*	19,98	28,00	30,00	30,00
Formsteel, Svelte 80	Trapezoidal	80	83	Longitudinal	X-HVB 140	*	*	*	*	21,97
Hibond 80	Trapezoidal	80	95	Longitudinal	X-HVB 140	*	*	*	*	16,07
Hibond 55	Trapezoidal	55	55	Longitudinal	X-HVB 95	*	28,00	28,00	30,00	30,00
Tray-dec 60	Trapezoidal	60	60	Longitudinal	X-HVB 95	*	21,32	28,00	30,00	30,00
Tray-dec 80	Trapezoidal	80	80	Longitudinal	X-HVB 125	*	*	*	18,00	24,14
ComFlor 60	Trapezoidal	60	75	Longitudinal	X-HVB 110	*	*	15,12	23,14	30,00
ComFlor 80	Trapezoidal	80	95	Longitudinal	X-HVB 140	*	*	*	*	12,12
ComFlor SR	Re-entrant	55	55	Longitudinal	X-HVB 95	*	28,00	28,00	30,00	30,00

### Spacing:

The spacing provisions as given in Annex B8 of ETA-15/0876 [2] apply.

# 2.5 FIRE RESISTANCE

Table 6 of Annex C5 of ETA-15/0876 [2] provides temperature dependent strength reduction factors  $k_{u,\Theta,X-HVB}$  for calculation of the X-HVB design resistance in case of a fire. The same reduction factors have been implemented within the "HERA Composite Beam and Slab Software".



# 3 LITERATURE AND APPENDICES

# 3.1 LITERATURE

- [1] AS/NZ 2327:2017 Composite structures composite steel-concrete construction in buildings. Standard Australia International/Standards New Zealand, Sydney/Wellington
- [2] ETA-15/0876: Design rules for Hilti Nailed Shear Connector X-HVB, HERA Report SSTR-066, Heavy Engineering Research Association, HERA ISBN 0112-1758, 12/12/2018
- [3] Hicks, S., Cao, J. (2019): *Design rules for Hilti Nailed Shear Connector X-HVB,* HERA Report SSTR-066, Heavy Engineering Research Association, HERA ISBN 0112-1758, 12/12/2018
- [4] EN 1994-1-1:2004 Eurocode 4: Design of composite steel and concrete structures Part 1.1.: General rules and rules for buildings, European Committee for Standardization, Brussels

# 3.2 APPENDICES

Appendix 1:	Sketches of geometries of the decking covered in the HERA-Software	page 1 to 3
Appendix 2:	Sketches of X-HVB positioning in ComFlor decking	page 1 to 7



## Geometry of Steel decking covered by the "HERA Composite Beam and Slab Software"

#### **Formsteel Unifloor**



#### Flatdeck



### Tray-dec 300



#### Svelte 60



#### Svelte 80





#### Hibond 80



#### Hibond 55



### Tray-dec 60



### Tray-dec 80





### ComFlor SR



#### ComFlor 60-600



### ComFlor 80-600





# X-HVB positioning drawings in ComFlor composite decking

#### **ComFlor SR**



#### ComFlor 60-600



### ComFlor 80-600





#### X-HVB positioned in Comflor-SR - Orientation: Longitudinal with the beam

Decking transverse with beam, 1 X-HVB per rib



Decking transverse with beam, 2 X-HVB per rib





#### X-HVB positioned in Comflor-SR - Orientation: Longitudinal with the beam

Decking transverse with beam, 3 X-HVB per rib





#### X-HVB positioned in Comflor 60-600 - Orientation: Transverse

Decking transverse with beam, 1 X-HVB per rib



Decking transverse with beam, 2 X-HVB per rib



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#### X-HVB positioned in Comflor 60-600 - Orientation: Transverse

Decking transverse with beam, 3 X-HVB per rib





#### X-HVB positioned in Comflor 80-600 - Orientation: Transverse

Decking transverse with beam, 1 X-HVB per rib



#### Decking transverse with beam, 2 X-HVB per rib



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#### X-HVB positioned in Comflor 80-600 - Orientation: Transverse

Decking transverse with beam, 3 X-HVB per rib



Decking transverse with beam, 4 X-HVB per rib



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Approval body for construction products and types of construction

#### **Bautechnisches Prüfamt**

An institution established by the Federal and Laender Governments



# European Technical Assessment

# ETA-15/0876 of 3 June 2016

English translation prepared by DIBt - Original version in German language

#### **General Part**

Technical Assessment Body issuing the European Technical Assessment:

Trade name of the construction product

Product family to which the construction product belongs

Manufacturer

Manufacturing plant

This European Technical Assessment contains

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of Deutsches Institut für Bautechnik

Nailed Shear Connector X-HVB

Nailed shear connector

Hilti AG Feldkircherstraße 100 9494 Schaan FÜRSTENTUM LIECHTENSTEIN

Plant 1 Plant 2

20 pages including 15 annexes which form an integral part of this assessment

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Deutsches Institut für Bautechnik

Kolonnenstraße 30 B | 10829 Berlin | GERMANY | Phone: +49 30 78730-0 | Fax: +49 30 78730-320 | Email: dibt.@ dibt.de | www.dibt.de



#### European Technical Assessment ETA-15/0876 English translation prepared by DIBt

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#### Specific part

#### 1 Technical description of the product

The nailed shear connector X-HVB is a mechanically attached shear connector for use in steel-to-concrete composite beams and in composite decks with profiled sheeting as an alternate to welded headed studs.

The nailed shear connector consists of an L-shaped cold-formed cantilever metal connector made from steel sheeting with a thickness of 2 mm or 2.5 mm. The cantilever metal part consists of a fastening leg and an anchorage leg. The fastening leg of the connector is fastened by 2 powder-actuated fasteners X-ENP-21 HVB to the steel member, whereas the anchorage leg embeds in the concrete deck of the composite beam. The nailed shear connector can be used for composite beams with and without profiled composite decking.

The height of the anchorage leg varies in order to take the different thicknesses of the concrete slab as well as the different heights of composite deck into account.

The different models of the X-HVB are:

X-HVB 140, X-HVB 125, X-HVB 110, X-HVB 95, X-HVB 80, X-HVB 50 and X-HVB 40.

The number in the product designation refers to the height of the X-HVB connector.

The powder-actuated fasteners X-ENP-21 HVB are made of zinc plated carbon steel. The fasteners comprise of a pin with a shank diameter of 4.5 mm and they are assembled with two metal washers. The washers serve to guide the fastener while it is being driven into the base material and they contribute to the shear resistance. The powder-actuated fastening tools Hilti DX 76 or Hilti DX 76 PTR are used in order to install the X-ENP-21 HVB together with the X-HVB shear connector. The driving force of the fastening tool is provided by the power load of the cartridge. The application limit of the powder-actuated fastening system depends on the strength and thickness of the base material. The fastening tools (incl. cartridges) are an integral part of this assessment with regard to the capacity of the nailed shear connector X-HVB and the application of the respective system.

The nailed shear connectors can be placed in one or more rows along the length of the composite beams. Aside of the use as shear connector for composite beams, nailed shear connectors may also be used for the end anchorage of composite decks, see Annex A1.

The shear connectors X-HVB and the powder-actuated fastener X-ENP-21 HVB are detailed in Annexes A1 and A2.

# 2 Specification of the intended use in accordance with the applicable European Assessment Document

The nailed shear connector X-HVB is intended to be used as connection device between steel and concrete in composite beams and composite decks according to EN 1994-1-1. The nailed shear connector can either be used in new buildings or for the renovation of existing buildings with the aim to increase the bearing capacity of aged floor constructions.

Shear connections of composite structures subject to static and quasi-static loading.

As the X-HVB is a ductile shear connector according to EN 1994-1-1, section 6.6, seismic loading is covered if the X-HVB is used as shear connector in composite beams used as secondary seismic members in dissipative as well as non-dissipative structures according to EN 1998-1.

The intended use is also specified in Annex A1 and B1 to B4.

Positioning of the connectors follows Annexes B5 to B8.

The installation is only carried out according to the manufacturer's instructions.



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In combination with composite decking the steel sheeting is in direct contact with the steel base material in the area of the connection.

Cartridge selection and tool energy settings in order to match the application limit diagram are taken into account.

Installation tests are carried out (e.g. check of nail head standoff  $h_{NVS}$ ), provided the fitness of the recommended cartridge cannot be checked otherwise.

The performances given in Section 3 are only valid if the nailed shear connector is used in compliance with the specifications and conditions given in Annexes B1 to B8.

The verifications and assessment methods on which this European Technical Assessment is based lead to the assumption of a working life of the nailed shear connector of at least 50 years. The indications given on the working life cannot be interpreted as a guarantee given by the producer, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

#### 3 Performance of the product and references to the methods used for its assessment

#### 3.1 Mechanical resistance and stability (BWR 1)

Essential characteristic	Performance
Characteristic resistance in solid concrete decks, shear connector orientation parallel to beam axis	See Annex C1
Characteristic resistance in solid concrete decks, shear connector orientation perpendicular to beam axis	No performance determined
Characteristic resistance in composite decks – decking ribs perpendicular to beam axis – shear connector orientation parallel or perpendicular to beam axis	See Annex C1
Characteristic resistance in composite decks – decking ribs parallel to beam axis – shear connector orientation parallel to beam axis	See Annex C2
Characteristic resistance in composite decks – decking ribs parallel to beam axis – shear connector orientation perpendicular to beam axis	No performance determined
Characteristic resistance of end anchorage of composite decks	See Annex C4
Characteristic resistance for use in seismic areas under seismic actions according to EN 1998-1	See Annex B1
Characteristic resistance in solid concrete decks in renovation application with old metallic iron or steel material with an actual yield strength less than 235 MPa	See Annex C3
Application limit	See Annex B3, pass



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#### 3.2 Safety in case of fire (BWR 2)

Essential characteristic	Performance			
Reaction to fire	Class A1 according to EN 13501-1:2007+A1:2009			
Resistance to fire	See Annex C5			

#### 3.3 Hygiene, health and the environment (BWR 3)

Essential characteristic	Performance
Content and/or release of dangerous substances	no performance determined

# 4 Assessment and verification of constancy of performance (AVCP) system applied, with reference to its legal base

In accordance with EAD No. 200033-00-0602, the applicable European legal act is: Decision 1998/214/EC.

The system to be applied is: 2+

# 5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited with Deutsches Institut für Bautechnik.

Issued in Berlin on 3 June 2016 by Deutsches Institut für Bautechnik

Uwe Bender Head of Department *beglaubigt:* Stöhr









#### **Table 1: Materials**

Designation	Material
Shear connector X-HVB	Steel DC04 of a thickness of 2 or 2.5 mm according to EN 10130, zinc plating $\ge$ 3 $\mu$ m
Powder-actuated fastener X-ENP-21 HVB	<ul> <li>Nail: Carbon steel C67S in keeping with EN 10132-4, quenched, tempered and galvanized.</li> <li>Nominal hardness: 58 HRC, Zinc plating ≥ 8 μm</li> <li>Washer: Steel DC01 according to EN 10139, zinc plating ≥ 10 μm</li> </ul>

#### Powder-actuated fastener X-ENP-21 HVB



#### Nailed shear connector X-HVB

Dimensions and materials

Annex A2



## Specification of intended use

The nailed shear connector X-HVB is intended to be used as connection device between steel and concrete in composite beams and composite decks according to EN 1994-1-1. The nailed shear connector can either be used in new buildings or for the renovation of existing buildings with the aim to increase the bearing capacity of aged floor constructions.

#### Shear connections of composite structures subject to:

- Static and quasi-static loading.
- As the X-HVB is a ductile shear connector according to EN 1994-1-1, section 6.6, seismic loading is covered if the X-HVB is used as shear connector in composite beams used as secondary seismic members in dissipative as well as non-dissipative structures according to EN 1998-1.

#### **Base materials:**

- Structural steel S235, S275 and S355 in qualities JR, JO, J2, K2 according to EN 10025-2, thickness see Annex B3.
- Old steels which cannot be classified accordingly are still applicable provided these are made of unalloyed carbon steel with minimum yield strength f<sub>y</sub> of 170 N/mm<sup>2</sup>.

#### Concrete:

- Normal weight concrete C20/25 C50/60 according to EN 206, minimum slab thickness see Annex B4.
- Light weight concrete LC 20/22 LC 50/55 according to EN 206 with a raw density ρ ≥ 1750 kg/m<sup>3</sup>, minimum slab thickness see Annex B4.

#### Composite decking:

• Steel for profiled sheeting follows EN 1993-1-3 and the material codes given there.

#### Design:

- · Design of the composite beams with X-HVB shear connectors is made according to EN 1994-1-1.
- The X-HVB shear connectors are ductile shear connectors according to EN 1994-1-1, section 6.6.
- The partial safety factor of  $\gamma_V = 1.25$  is used provided no other values are given in national regulations of the member states.

#### Installation:

- The installation is only carried out according to the manufacturer's instructions.
- In combination with composite decking the steel sheeting is in direct contact with the steel base material in the area of the connection.
- Cartridge selection and tool energy settings in order to match the application limit diagram are taken into account, see Annex B3.
- Installation tests are carried out (e.g. check of nail head standoff h<sub>NVS</sub>), provided the fitness of the recommended cartridge cannot be checked otherwise.

#### Nailed shear connector X-HVB

Specification of intended use

Annex B1









## Fastener inspection







Maximum total thickness of fixed sheeting t<sub>fix</sub> 2.0 mm for X-HVB 80, X-HVB 95 and X-HVB 110 1.5 mm for X-HVB 125 and X-HVB 140

### Minimum slab thickness

	Minimum slab thickness h [mm]		
X-HVB	Without effect of corrosion	With effect of corrosion	
40	50	60	
50	60	70	
80	80	100	
95	95	115	
110	110	130	
125	125	145	
140	140	160	



## Maximum decking height hp dependent on decking geometry

	Maximum height of composite decking hp [mm]			
X-HVB	<u>b₀</u> h <sub>p</sub> ≥ 1.8	$1.0 < \frac{b_0}{h_p} < 1.8$	$\frac{b_0}{h_p} \le 1.0^{\times)}$	
80	45	45	30	
95	60	57	45	
110	75	66	60	
125	80	75	73	
140	80	80	80	

<sup>x)</sup>  $b_0/h_p \ge 1$  for composite decking perpendicular to beam combined with X-HVB orientation parallel with beam

#### Nailed shear connector X-HVB

Annex B4

Geometric parameters









# Minimum rib width and spacing to decking in case of single row positioning



# Minimum rib width in case of multiple row positioning







## Positioning in one row with composite deck with or without rib stiffener



# Positioning in two or three rows







### Nailed shear connector X-HVB

Positioning in composite beams with composite decking parallel with beam axis Annex B8



Shear Connector	Characteristic Resistance P <sub>Rk</sub> [kN]	Design Resistance P <sub>Rd</sub> [kN]	Minimum base material thickness [mm]	X-HVB positioning <sup>3)</sup>	Ductility assessment
X-HVB 40	29	23	6	"desslars all ?"	
X-HVB 50	29	23	6	duckwaik	
X-HVB 80	32.5	26	a	Ductile	
X-HVB 95	35	28		parallel with beam	according to EN
X-HVB 110	35	28	8 <sup>2)</sup>		with 1994-1-1
X-HVB 125	37.5	30	]		
X-HVB 140	37.5	30	1		

<sup>1)</sup> In the absence of other national regulations a partial safety factor  $\gamma_V = 1.25$  applies

<sup>2)</sup> Reduction to 6 mm minimum base material thickness possible, see Annex C3

<sup>3)</sup> "Duckwalk" positioning according to Annex C3, positioning "parallel with beam" according to Annex B5

#### Conditions:

- Normal weight concrete C20/25 to C50/60
- Light weight concrete LC20/22 to LC50/55 with a minimum density ρ = 1750 kg/m<sup>3</sup>
- Observation of positioning rules according to Annex B5 and Annex C3

#### Table 4: Design resistance in composite beams with decking ribs transverse to beam axis

X-HVB positioning	Design Resistance P <sub>Rd,t</sub>	Ductility assessment
X-HVB positioning longitudinal with the beam	$P_{Rd,t,l} = k_{t,l} \cdot P_{Rd}$ $k_{t,l} = \frac{0.66}{\sqrt{n_r}} \cdot \frac{b_0}{h_p} \cdot \left(\frac{h_{SC}}{h_p} - 1\right) \le 1.0$	Ductile
X-HVB positioning transverse with the beam	$P_{Rd,t,t} = 0.89 \cdot k_{t,t} \cdot P_{Rd}$ $k_{t,t} = \frac{1.18}{\sqrt{n_r}} \cdot \frac{b_0}{h_p} \cdot \left(\frac{h_{SC}}{h_p} - 1\right) \le 1.0$	according to EN 1994-1-1

Conditions:

- Design resistance P<sub>Rd</sub> for solid concrete slabs according to Table 3
- Normal weight concrete C20/25 to C50/60
- Light weight concrete LC20/22 to LC50/55 with a minimum raw density  $\rho = 1750 \text{ kg/m}^3$
- Geometric parameters b<sub>0</sub>, h<sub>p</sub> and h<sub>SC</sub> according to Annex B4, n<sub>r</sub> corresponds to the number of X-HVBs per rib
- Observation of positioning rules according to Annex B6 and Annex B7
- Applicable for X-HVB 80, X-HVB 95, X-HVB 110, X-HVB 125, X-HVB 140

#### Nailed shear connector X-HVB

Characteristic and design values of resistance:

Solid concrete slabs and composite slabs with decking transverse to beam

Annex C1



Table 5: Design resistance in composite beams with decking ribs parallel to beam axis			
X-HVB positioning	Design Resistance P <sub>Rd,I</sub>	Ductility assessment	
≥20 mm ≥50 mm ≥50 mm X-HVB positioning longitudinal with the beam	$P_{Rd,l} = k_l \cdot P_{Rd}$ $k_l = 0.6 \cdot \frac{b_0}{h_p} \cdot \left(\frac{h_{SC}}{h_p} - 1\right) \le 1.0$	Ductile according to EN 1994-1-1	

Conditions:

- Design resistance P<sub>Rd</sub> for solid concrete slabs according to Annex C1, Table 3
- X-HVB are to be positioned parallel with beam
- Normal weight concrete C20/25 to C50/60
- Light weight concrete LC20/22 to LC50/55 with a minimum density  $\rho = 1750 \text{ kg/m}^3$
- Geometric parameters  $b_0$ ,  $h_p$  and  $h_{SC}$  according to Annex B4
- Observation of positioning rules according to Annex B8
- Applicable for X-HVB 80, X-HVB 95, X-HVB 110, X-HVB 125, X-HVB 140

#### Nailed shear connector X-HVB

Characteristic and design values of resistance: Composite slabs with decking parallel to beam Annex C2



## Design resistance: Effect of reduced base material thickness for X-HVB 80 to X-HVB 140

Reduction of design resistance  $P_{Rd}$  with the factor ( $t_{II,act}$  / 8) is required in case the actual base material thickness is less than 8 mm.

$$P_{Rd,red} = \frac{t_{II,act}}{8} \cdot P_{Rd} \ge 23.0 \ kN$$

with:

P<sub>Rd</sub> ..... design resistance in solid concrete slab of X-HVB 80 to X-HVB 140 according to Annex C1, Table 3

Notes: Corresponding values can also be applied in new construction. No extrapolation of above formula for base material thickness  $t_{II} > 8$  mm

## Design resistance: Effect of reduced base material strength

Reduction of design resistance  $P_{Rd}$  with the factor  $\alpha_{BM,red}$  is required in case the actual base material  $f_u$  strength of the old construction steel is less than 360 N/mm<sup>2</sup>.

Minimum ultimate strength  $f_{u,min} = 300 \text{ N/mm}^2$  (with a minimum yield strength  $f_y = 170 \text{ N/mm}^2$ )

$$P_{Rd,red} = \alpha_{BM,red} \cdot P_{Rd}$$

 $\alpha_{BM,red} = 0.95$ 

with:

 $P_{Rd,red}$  .... reduced design strength of X-HVB for base material strength between 300 and 360 N/mm<sup>2</sup>  $P_{Rd}$  ...... design resistance of X-HVB according to Annex C1, Table 3 and Table 4

 $\alpha_{\text{BM,red}}...$  base material strength reduction factor

# "Duckwalk" positioning of X-HVB 40 and 50 in combination with thin solid slabs:







Annex C4



able 6: Temperature dependent strength reduction facto				
	Temperature of top flange <sub>Øx-HVB</sub> [°C]	k <sub>u,⊕,X-HVB</sub>		
	20	1.00		
	100	1.00		
	200	0.95		
	300	0.77		
	400	0.42		
	500	0.24		
	600	0.12		
	≥ 700	0		

#### T r

The design of the X-HVB shear connector in case of a fire is done according to EN 1994-1-2. The reduction factor k<sub>u.e.X-HVB</sub> shall be determined with the temperature of the steel top flange to which the X-HVB is connected.

The characteristic resistance of the X-HVB nailed shear connector at elevated temperature is calculated:

In case of solid concrete slabs:

$$P_{fi,Rk} = k_{u,\theta,X-HVB} \cdot P_{Rk}$$

with:

Pfi.Bk .... characteristic resistance of X-HVB shear connector at elevated temperature. characteristic resistance of X-HVB shear connector according to Annex C1, Table 3. P<sub>Bk</sub> ....

In case of composite beams with decking ribs transverse to the beam:

 $P_{fi,Rk} = k_{u,\theta,X-HVB} \cdot k_{t,l} \cdot P_{Rk}$  or  $P_{fi,Rk} = 0.89 \cdot k_{u,\theta,X-HVB} \cdot k_{t,t} \cdot P_{Rk}$ with:

characteristic resistance of X-HVB shear connector at elevated temperature. P<sub>fi.Bk</sub> .... characteristic resistance of X-HVB shear connector according to Annex C1, Table 3 P<sub>Rk</sub> .... ktl or ktt ... reduction factor according to Annex C1, Table 4

In case of composite beams with decking ribs parallel to the beam:

$$P_{fi,Rk} = k_{u,\theta,X-HVB} \cdot k_l \cdot P_{Rk}$$

with:

P<sub>fi,Rk</sub> .... characteristic resistance of X-HVB shear connector at elevated temperature. characteristic resistance of X-HVB shear connector according to Annex C1, Table 3 P<sub>Rk</sub> .... reduction factor according to Annex C2, Table 5 k<sub>l</sub> ...

 $k_{u,\Theta,X-HVB}$  temperature dependent reduction factor according to Table 6.

The design resistance of the X-HVB nailed shear connector at elevated temperature is calculated as follows:

$$P_{fi,Rd} = \frac{1}{\gamma_{M,fi,V}} \cdot P_{fi,Rk}$$

with

 $\gamma_{M,fi,V}$  .... partial safety factor in case of a fire, in the absence of national regulations  $\gamma_{M,fi,V} = 1.0$  applies

#### Nailed shear connector X-HVB

Annex C5

Characteristic and design resistance to fire